



## Regenerable ceria-based SO<sub>x</sub> traps for sulfur removal in lean exhausts

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### ABSTRACT

Bare and Pt-containing CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>:MgO mixed oxide and Al<sub>2</sub>O<sub>3</sub> have been investigated as potential regenerable sulfur oxides (SO<sub>x</sub>) traps. The samples were evaluated by lean SO<sub>x</sub> adsorption and temperature programmed desorption using synthetic gas compositions. In addition, combined DRIFT spectroscopy and mass spectrometry were employed to obtain mechanistic information on the adsorption of SO<sub>x</sub>. The results suggest Pt/CeO<sub>2</sub> as promising SO<sub>x</sub> trap material owing to a high storage capacity at 250 °C in combination with efficient release above 600 °C. The presence of Pt is generally found to enhance the lean SO<sub>x</sub> storage capacity at 250 °C for CeO<sub>2</sub>-based samples. Lean SO<sub>2</sub> adsorption on CeO<sub>2</sub> is found to proceed via the formation of surface and bulk sulfates, where the latter is formed more rapidly for the Pt-containing CeO<sub>2</sub> sample. Ceria samples pre-exposed to high amounts of SO<sub>2</sub> at 250 and 400 °C show lower SO<sub>x</sub> storage capacity and higher SO<sub>x</sub> release as compared to fresh samples. This indicates that under the conditions used in this study, a part of the storage sites on CeO<sub>2</sub> are non-regenerable.

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### 1. Introduction

One strategy to reduce CO<sub>2</sub> emissions within the transportation sector is to increase the fuel efficiency by the use of lean-burn or diesel engines [1]. The lean character of the exhausts from these engines requires other aftertreatment concepts than standard three-way technology. One such concept is NO<sub>x</sub> storage catalysis which has shown promising characteristics for NO<sub>x</sub> reduction under net-lean conditions [2]. This concept is based on temporary storage of NO<sub>x</sub> on basic storage sites, usually provided by metal oxides like barium oxide (BaO), during lean periods and release with subsequent reduction of NO<sub>x</sub> over noble metals during short periods of rich or stoichiometric conditions. However, one issue regarding this type of catalyst is the sensitivity of the storage material to sulfur, i.e., high affinity towards storage of sulfur oxides (SO<sub>x</sub>) under lean conditions and negligible release of sulfur compounds under the NO<sub>x</sub> regeneration phase. In course of time, a progressing sulfur poisoning will reduce the NO<sub>x</sub> storage capacity and the number of available NO<sub>x</sub> storage sites will eventually become critically low, which leads to insufficient NO<sub>x</sub> storage and reduction [2–5]. To regenerate the NO<sub>x</sub> storage capacity at this stage, thermal decomposition under net reducing conditions by a drastic increase of temperature is essentially the only solution.

However, the temperature required for this procedure is too high to guarantee the stability of the catalyst towards thermal deactivation.

Sulfur containing species in the exhausts originate from fuel and lubricants. Even though the content of sulfur in the fuel has been significantly reduced over the years, the presence of sulfur will always lead to reduced NO<sub>x</sub> storage capacity. Thus, within the present technology, strategies to handle sulfur in the exhaust are necessary. This can be achieved by increasing the sulfur tolerance of the aftertreatment system or preventing SO<sub>x</sub> from reaching the NO<sub>x</sub> storage catalyst by using upstream SO<sub>x</sub> traps. The sulfur tolerance of the catalyst can be increased by enhancing the release of sulfur species during regeneration and/or by decreasing the sulfur affinity of the storage material. The sulfur release during regeneration can, for example, be facilitated by using thinner washcoat layers [6] or by adding TiO<sub>2</sub> to the Al<sub>2</sub>O<sub>3</sub>-support of the NO<sub>x</sub> storage catalyst [1]. Moreover, the amount of sulfur adsorbed can be decreased by replacing the NO<sub>x</sub> storing component with a material with lower affinity towards sulfur compounds [7,8]. A few different SO<sub>x</sub> trap strategies have been suggested and materials such as BaO supported on Al<sub>2</sub>O<sub>3</sub> [9], Ba/Cu-benzene tricarboxylate [10], K<sub>x</sub>Mn<sub>8</sub>O<sub>16</sub> [11] and MnO [12] have been proposed as SO<sub>x</sub> adsorbents.

In the present work, a series of different materials is evaluated as regenerable SO<sub>x</sub> traps. Such traps should, in different temperature intervals, store and release SO<sub>x</sub> under lean conditions. During regeneration of the SO<sub>x</sub> trap, the exhausts will be by-passed

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the NO<sub>x</sub> storage catalyst to minimize the sulfur exposure. This strategy should be chosen as sulfur species previously have been reported to adsorb on the catalyst under both lean and rich conditions blocking storage and noble metal sites [13]. To our knowledge, this regeneration technique has not previously been suggested in the literature. The desired properties of the SO<sub>x</sub> adsorbent are to store SO<sub>x</sub> under normal lean exhaust conditions in the temperature interval 200–500 °C and release the stored sulfur species under lean conditions at temperatures slightly above 500 °C. In this way, the fuel consumption required to produce the heat for regeneration is minimized. To avoid permanent sulfur poisoning, we intuitively choose to compare different metal oxides that are sufficiently basic to store SO<sub>x</sub>, e.g. CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>:MgO mixed oxide and Al<sub>2</sub>O<sub>3</sub>, but less basic than BaO. Ceria is an interesting oxide for many aftertreatment applications. For example, ceria is used as an oxygen storage component in the three-way catalyst and as SO<sub>x</sub> traps for stationary applications [14]. It is known that sulfates may form on ceria upon exposure to SO<sub>2</sub> even in the absence of oxygen [15], a property that probably is caused by the high oxygen mobility within the material. Adsorbents based on Al<sub>2</sub>O<sub>3</sub>:MgO mixed oxides from hydrotalcite precursors have also been suggested as SO<sub>x</sub> traps for stationary applications [16]. By using hydrotalcite precursors for the mixed oxide, it is possible to control the basicity of the storage material by varying the Al<sub>2</sub>O<sub>3</sub>:MgO ratio. Alumina, which is an amphoteric oxide, is the least basic oxide in the present study and is included primarily as reference material. Boehmite is used as binder for the monolith samples which means that all samples contain some Al<sub>2</sub>O<sub>3</sub>. To investigate the suitability of these metal oxides as SO<sub>x</sub> traps, we have employed both kinetic studies in a flow-reactor and mechanistic studies by combined qualitative diffuse reflectance infrared fourier transformed spectroscopy (DRIFTS) and mass spectrometry. The influence of noble metal on the SO<sub>x</sub> storage and release properties of the SO<sub>x</sub> traps is investigated as well as the stability of the SO<sub>x</sub> adsorbent.

## 2. Experimental considerations

### 2.1. Sample preparation and characterisation

The metal oxides used as SO<sub>x</sub> adsorbents were; CeO<sub>2</sub> (99.5 H.S.A. 514, Rhône-Poulenc), Al<sub>2</sub>O<sub>3</sub>:MgO (30:70 wt.%) mixed oxide prepared from a hydrotalcite precursor (Condea) and Al<sub>2</sub>O<sub>3</sub> (Puralox SBA-200, Sasol). All samples were pre-treated in air at 750 °C for 2 h. The Pt-containing powder samples were prepared by wet impregnation of Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> using Pt(NO<sub>3</sub>)<sub>2</sub> (Hereaus) as precursor. Due to different point of zero charge for the oxides, the impregnation was performed at pH 2 and 3 for the Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> sample, respectively. After impregnation, the slurries were instantly frozen with liquid nitrogen and freeze-dried. The resulting powder samples were finally calcined in air at 600 °C for 1 h (heating rate of 4.8 °C/min from 25 to 600 °C). Surface area measurements of the powder samples were performed by N<sub>2</sub>-physisorption at 77 K using a Micromeritics Tristar instrument. For a few selected samples, the specific surface areas, calculated using the BET-method [17], are summarised in Table 1.

Monoliths samples (Ø = 20 mm and length = 20 mm) were cut from a commercial honeycomb cordierite structure with 400 cpsi. The monoliths were coated with the SO<sub>x</sub> adsorbent material following the procedure described in Ref. [18]. As a binder for the adsorbent material, Boehmite (Disperal SOL P2, Condea) was used in all samples (20 wt.% of the dry material in the slurry). After coating, all monolith samples were calcined in air at 650 °C for 3 h. The Pt-containing samples were prepared by impregnation of the coated monoliths using Pt(NO<sub>3</sub>)<sub>2</sub> as platinum precursor for the

**Table 1**

Specific surface area of Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub>-based powder samples

Sample	Specific surface area (m <sup>2</sup> /g)	Comment
CeO <sub>2</sub>	254	Fresh
CeO <sub>2</sub>	82	Air, 750 °C, 2 h
5 wt.% Pt/CeO <sub>2</sub>	78	CeO <sub>2</sub> treated in air, 750 °C, 2 h and impregnated with Pt
Al <sub>2</sub> O <sub>3</sub>	203	Fresh
Al <sub>2</sub> O <sub>3</sub>	187	Air, 750 °C, 2.5 h
5 wt.% Pt/Al <sub>2</sub> O <sub>3</sub>	174	Al <sub>2</sub> O <sub>3</sub> treated in air, 750 °C, 2.5 h and impregnated with Pt

Al<sub>2</sub>O<sub>3</sub> and CeO<sub>2</sub> samples and Pt(NH<sub>3</sub>)<sub>2</sub>(NO<sub>2</sub>)<sub>2</sub> (Johnson Matthey) for the Al<sub>2</sub>O<sub>3</sub>:MgO sample. The impregnation was performed at pH 2, 3 and 8 for the Al<sub>2</sub>O<sub>3</sub>, CeO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>:MgO sample, respectively. After impregnation, the monolith samples were dried in air at 80 °C for 12 h. The temperature was thereafter gently increased by 4.3 °C/min to 600 °C and the samples were finally calcined in air at this temperature for 1 h.

### 2.2. Isothermal SO<sub>2</sub> adsorption followed by temperature programmed desorption

The flow-reactor experiments with monolith samples were performed using a quartz tube reactor equipped with a gas mixer unit (Environmentics 2000) for control of the inlet gas composition, and a surrounding metal coil for resistive heating of the reactor tube. A thermocouple (type K, Pentronic) placed 10 mm upstream of the monolith was used together with a Eurotherm regulator to control the inlet gas temperature. A second thermocouple was positioned inside the monolith, about 2 mm from the end of the sample, to measure the sample temperature. To facilitate the analysis of the total SO<sub>x</sub> outlet concentration, the experimental method previously reported by McLaughlin et al. [19] was used. Following this method, the outlet gas flow was first passed over an oxidation catalyst before introduced to the SO<sub>2</sub> analyser (non-dispersive IR, Maihak UNOR 610). For further information about the experimental method see Appendix A.

For all experiments, the total flow was 3500 ml/min, which corresponds to GHSV = 33 400 h<sup>-1</sup>, and Ar was used as balance. Prior to each experiment, the samples were treated in 7% O<sub>2</sub> for 10 min at 500 °C. The temperature was thereafter decreased and lean SO<sub>x</sub> adsorption was performed (100 ppm SO<sub>2</sub> and 7% O<sub>2</sub> in Ar) at 250 or 400 °C for 1 h. The high SO<sub>2</sub> concentration in these experiments was used to assure measurement accuracy rather than mimicking real lean exhaust conditions. After the SO<sub>2</sub> exposure, temperature programmed desorption (lean SO<sub>x</sub>-TPD) was performed by increasing the temperature by 10 °C/min to 700 °C in 7% O<sub>2</sub>. The temperature was kept constant at 700 °C for 20 min before cooling in Ar.

### 2.3. DRIFT spectroscopy measurements

FTIR measurements were performed with powder samples in diffuse reflectance mode using a Bio-Rad FTS6000 spectrometer equipped with a Harrick Praying Mantis DRIFTS cell and a MCT detector. The resolution was 1 cm<sup>-1</sup> and the number of scans per spectrum was set to 20. All experiments were performed with fresh samples using a total gas flow of 100 ml/min and Ar as balance. Prior to each experiment, the sample was treated in 20% O<sub>2</sub> at 500 °C for 10 min followed by cooling in 7% O<sub>2</sub> to the temperature to be studied, i.e., 250 or 400 °C. Because the windows in the reactor dome absorb IR radiation in the same wavenumber

**Table 2**  
Procedure during DRIFTS experiments

Step	Time (min)	Gas feed (Ar as balance)	Dome on/off	Comment
1	5	7% O <sub>2</sub>	On	Spectra recorded before SO <sub>2</sub> exposure
2	3	7% O <sub>2</sub>	Off	
3	5	7% O <sub>2</sub>	On	
4	5	300 ppm SO <sub>2</sub> and 7% O <sub>2</sub>	On	Spectra recorded after 5 min of SO <sub>2</sub> exposure
5	15	7% O <sub>2</sub>	On	
6	3	7% O <sub>2</sub>	Off	
7	3	7% O <sub>2</sub>	On	Spectra recorded after 10 min of SO <sub>2</sub> exposure
8	5	300 ppm SO <sub>2</sub> and 7% O <sub>2</sub>	On	
9	15	7% O <sub>2</sub>	On	
10	3	7% O <sub>2</sub>	Off	Spectra recorded after 20 min of SO <sub>2</sub> exposure
11	3	7% O <sub>2</sub>	On	
12	10	300 ppm SO <sub>2</sub> and 7% O <sub>2</sub>	On	
13	15	7% O <sub>2</sub>	On	Spectra recorded after 40 min of SO <sub>2</sub> exposure
14	3	7% O <sub>2</sub>	Off	
15	3	7% O <sub>2</sub>	On	
16	20	300 ppm SO <sub>2</sub> and 7% O <sub>2</sub>	On	Spectra recorded after 1 h of SO <sub>2</sub> exposure
17	15	7% O <sub>2</sub>	On	
18	3	7% O <sub>2</sub>	Off	
19	3	7% O <sub>2</sub>	On	Spectra recorded after 3 h of SO <sub>2</sub> exposure
20	20	300 ppm SO <sub>2</sub> and 7% O <sub>2</sub>	On	
21	15	7% O <sub>2</sub>	On	
22	3	7% O <sub>2</sub>	Off	Spectra recorded after 3 h of SO <sub>2</sub> exposure
23	3	7% O <sub>2</sub>	On	
24	120	300 ppm SO <sub>2</sub> and 7% O <sub>2</sub>	On	
25	15	7% O <sub>2</sub>	On	Spectra recorded after 3 h of SO <sub>2</sub> exposure
26	3	7% O <sub>2</sub>	Off	

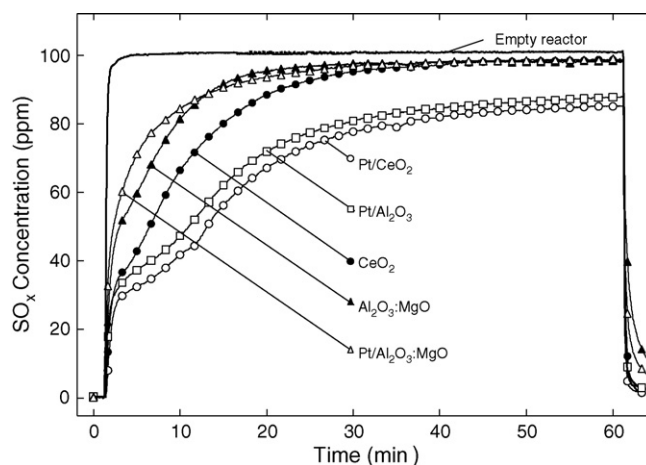
region as some sulfur species, the dome was removed during the recording of spectra. To manage this procedure while simultaneously facilitate the study of how different species are formed on the samples, the SO<sub>x</sub> adsorption experiments were performed as a sequence of several steps described in Table 2. During SO<sub>2</sub> exposure and subsequent flushing of the reaction cell, the dome was attached to the cell. After flushing, the dome was removed for 3 min and the spectra were recorded under continuous flushing of 7% O<sub>2</sub> in Ar at the adsorption temperature. By this procedure, sample exposure to air is minimized which also was confirmed by reference experiments without SO<sub>2</sub> exposure showing no detectable IR bands from species that possibly can originate from air contaminants.

### 3. Results

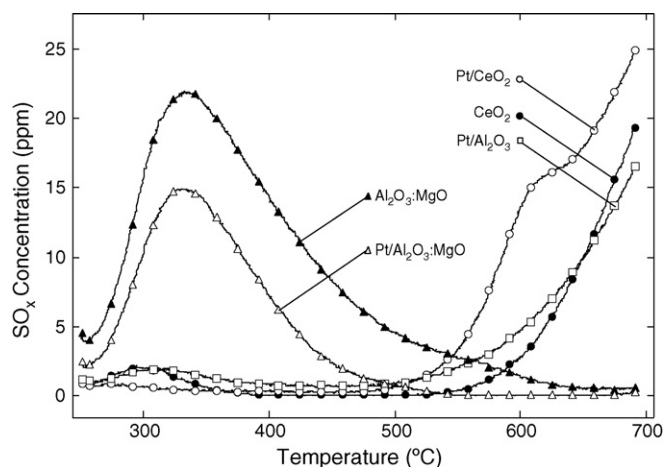
#### 3.1. Flow-reactor experiments

Fig. 1 shows the outlet SO<sub>x</sub> concentrations during lean SO<sub>x</sub> adsorption for the series of monolith samples (CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>:MgO, Pt/Al<sub>2</sub>O<sub>3</sub>, Pt/CeO<sub>2</sub> and Pt/Al<sub>2</sub>O<sub>3</sub>:MgO) at 250 °C. Repeated lean SO<sub>x</sub> adsorption at 250 °C followed by TPD experiments were performed and the results from the 7th cycle are displayed. As a reference, also the results for the corresponding experiments with empty reactor are included in the figure. With the assumption that the amount of SO<sub>x</sub> not reaching the detector is adsorbed on the sample, the area between the SO<sub>x</sub> signal for the empty reactor and the actual experiment in Fig. 1 is proportional to the SO<sub>x</sub> storage capacity. At  $t = 1$  min, 100 ppm SO<sub>2</sub> is introduced which results in a rapid increase of the SO<sub>x</sub> outlet concentration. After the initial phase, a twitch on the SO<sub>x</sub> signal to a slower increase in outlet SO<sub>x</sub> concentration can be seen for all samples. After the twitch, the most rapid increase is observed for the Al<sub>2</sub>O<sub>3</sub>:MgO-based samples and throughout the experiment the SO<sub>x</sub> signal for the Al<sub>2</sub>O<sub>3</sub>:MgO-based samples declines and

levels out close to the feed gas concentration around  $t = 30$  min. Compared to the Al<sub>2</sub>O<sub>3</sub>:MgO-based samples, the SO<sub>x</sub> signal for the CeO<sub>2</sub> sample increases somewhat slower after the twitch and the SO<sub>x</sub> concentration levels out close to the feed gas concentration around  $t = 40$  min. In the case of the Pt/CeO<sub>2</sub> and Pt/Al<sub>2</sub>O<sub>3</sub> samples, however, the characteristic of the SO<sub>x</sub> signal is different. The twitch to a slower increase of the outlet SO<sub>x</sub> concentration after the initial phase is significantly more pronounced and a second twitch appears around  $t = 10$  and 12 min for the Pt/Al<sub>2</sub>O<sub>3</sub> and Pt/CeO<sub>2</sub> samples, respectively. Thereafter, the increase in SO<sub>x</sub> concentration then declines for both samples although the SO<sub>x</sub> concentration never reaches the feed gas level during the experimental time (60 min).



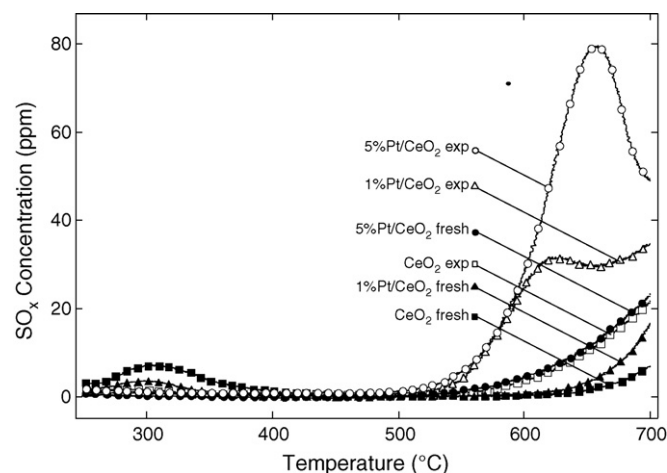
**Fig. 1.** SO<sub>x</sub> signals during SO<sub>2</sub> adsorption at 250 °C for CeO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>:MgO (30:70), Pt/Al<sub>2</sub>O<sub>3</sub>, Pt/CeO<sub>2</sub> and Pt/Al<sub>2</sub>O<sub>3</sub>:MgO samples. The response for the empty reactor is included as system reference. Active mass: 0.87 g/monolith sample. Feed composition during adsorption: 100 ppm SO<sub>2</sub> and 7% O<sub>2</sub> in Ar. GHSV: 33 400 h<sup>-1</sup>.



**Fig. 2.** Lean  $\text{SO}_x$ -TPD results for the  $\text{CeO}_2$ ,  $\text{Al}_2\text{O}_3\text{:MgO}$  (30:70),  $\text{Pt/Al}_2\text{O}_3$ ,  $\text{Pt/CeO}_2$  and  $\text{Pt/Al}_2\text{O}_3\text{:MgO}$  samples after  $\text{SO}_2$  adsorption at 250 °C. Feed composition during the TPD: 7%  $\text{O}_2$  in Ar. GHSV: 33 400  $\text{h}^{-1}$ . Ramp rate: 10 °C/min.

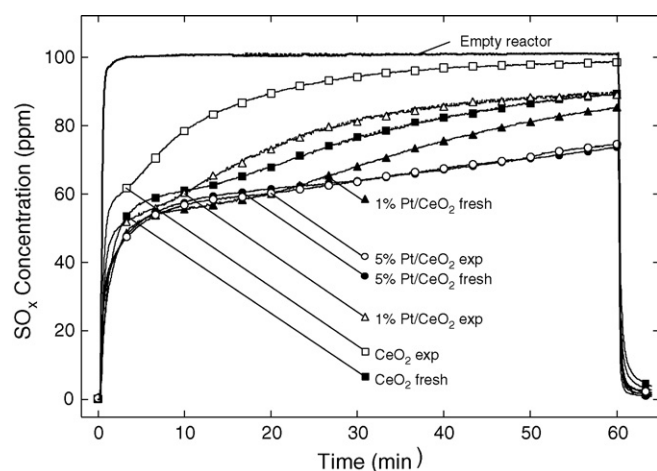
The results from the subsequent lean  $\text{SO}_x$ -TPD experiments are displayed in Fig. 2. For the  $\text{Al}_2\text{O}_3\text{:MgO}$  containing samples,  $\text{SO}_x$  desorption starts already at 260 °C and clear maxima are observed around 330 °C. No significant  $\text{SO}_x$  desorption is observed above 550 and 650 °C for the  $\text{Pt/Al}_2\text{O}_3\text{:MgO}$  and  $\text{Al}_2\text{O}_3\text{:MgO}$  samples, respectively. Except for minor desorption around 300 °C, no substantial  $\text{SO}_x$  desorption is detected below 500 °C for the  $\text{Al}_2\text{O}_3$  and  $\text{CeO}_2$ -based samples. Instead,  $\text{SO}_x$  desorption starts at temperatures slightly above 500 °C and increases rapidly at about 550 °C, especially for the  $\text{Pt/CeO}_2$  sample. A special feature for the  $\text{Pt/CeO}_2$  sample is the well-pronounced shoulder on the  $\text{SO}_x$  signal at around 600 °C. The  $\text{Pt/Al}_2\text{O}_3$ ,  $\text{Pt/CeO}_2$  and  $\text{CeO}_2$  samples all show the highest desorption at 700 °C which is the maximum temperature during the experiment.

The lean  $\text{SO}_x$  storage and TPD results indicate that  $\text{Pt/CeO}_2$  is a promising  $\text{SO}_x$  trap material and that the presence of Pt significantly influences the performance of  $\text{CeO}_2$ -based  $\text{SO}_x$  traps. Therefore, further studies were performed to investigate the  $\text{SO}_x$  adsorption and regeneration properties of  $\text{CeO}_2$ -based  $\text{SO}_x$  traps containing 0, 1 and 5 wt.% Pt. Figs. 3 and 4 show the results from the lean  $\text{SO}_x$  adsorption and subsequent  $\text{SO}_x$ -TPD experiments

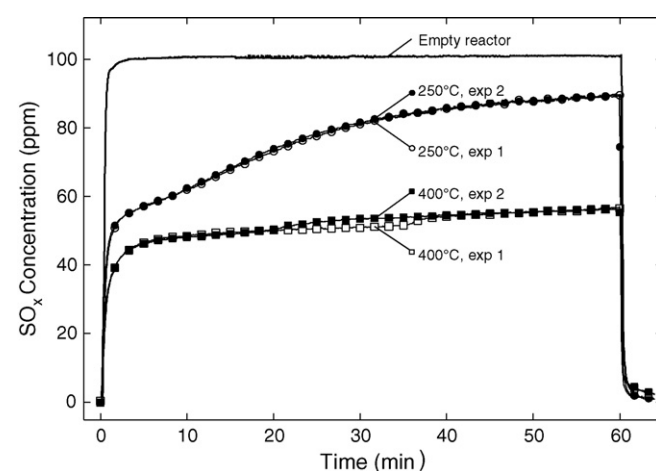


**Fig. 4.** Lean  $\text{SO}_x$ -TPD results for fresh and  $\text{SO}_2$  pre-exposed  $\text{CeO}_2$ -based samples containing 0, 1 and 5 wt.% Pt, respectively after  $\text{SO}_2$  adsorption at 250 °C. Feed composition during the TPD: 7%  $\text{O}_2$  in Ar. GHSV: 33 400  $\text{h}^{-1}$ . Ramp rate: 10 °C/min.

(analogous to Figs. 1 and 2) for both fresh and  $\text{SO}_2$  pre-exposed  $\text{CeO}_2$ -based samples. With  $\text{SO}_2$  pre-exposed samples we refer to samples that in addition to the lean  $\text{SO}_x$  adsorption and TPD experiments have been exposed to 700 ppm  $\text{SO}_2$  and 7%  $\text{O}_2$  in Ar for 1 h first at 250 °C and then for 1 h at 400 °C. In order to remove  $\text{SO}_x$  from regenerable sites, a TPD is performed before starting the second lean  $\text{SO}_x$  adsorption and TPD experiment with the pre-exposed sample. During the  $\text{SO}_x$  adsorption (cf. Fig. 3), all samples have similar uptake performance as the  $\text{CeO}_2$  samples in Fig. 1. For the fresh samples the outlet  $\text{SO}_x$  concentration is generally lower during 1 h of lean  $\text{SO}_2$  exposure for samples with higher Pt loading. The same trend is observed for the  $\text{SO}_2$  pre-exposed samples. Comparing fresh and  $\text{SO}_2$  pre-exposed samples with the same Pt loading reveal that the outlet  $\text{SO}_x$  concentration is generally lower for the fresh samples. The only exception is the 5 wt.%  $\text{Pt/CeO}_2$  sample where the difference between fresh and  $\text{SO}_2$  pre-exposed samples is very small. Considering the lean  $\text{SO}_x$ -TPD, a small amount of  $\text{SO}_x$  desorbs already around 300 °C from the fresh 0 and 1 wt.%  $\text{Pt/CeO}_2$  samples. Desorption at this low temperature is neither observed for the 5 wt.%  $\text{Pt/CeO}_2$  sample nor for the pre-exposed samples. For the fresh samples, increased  $\text{SO}_x$  desorption

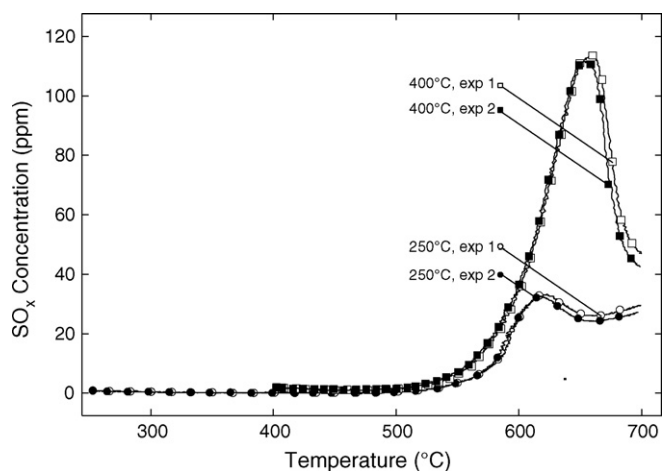


**Fig. 3.**  $\text{SO}_x$  signals during  $\text{SO}_2$  adsorption at 250 °C for fresh and  $\text{SO}_2$  pre-exposed  $\text{CeO}_2$ -based samples containing 0, 1 and 5 wt.% Pt, respectively. The response for the empty reactor is included as system reference. Active mass: 1.00 g/monolith sample. Feed composition during adsorption: 100 ppm  $\text{SO}_2$  and 7%  $\text{O}_2$  in Ar. GHSV: 33 400  $\text{h}^{-1}$ .



**Fig. 5.**  $\text{SO}_x$  signals during lean  $\text{SO}_2$  adsorption for repeated experiments for a 1 wt.%  $\text{Pt/CeO}_2$  sample. The  $\text{SO}_2$  adsorption temperature was alternated in the following sequence: 400, 250, 400 and 250 °C. The response for the empty reactor is included as system reference. Active mass: 1.00 g/monolith sample. Feed composition during adsorption: 100 ppm  $\text{SO}_2$  and 7%  $\text{O}_2$  in Ar. GHSV: 33 400  $\text{h}^{-1}$ .





**Fig. 6.**  $\text{SO}_x$  signals from the desorption part of the repeated lean  $\text{SO}_2$  adsorption and  $\text{SO}_x$ -TPD experiments performed with a 1 wt.% Pt/ $\text{CeO}_2$  sample. The  $\text{SO}_2$  adsorption temperature was alternated in the following sequence: 400, 250, 400 and 250 °C. Feed composition during the TPD: 7%  $\text{O}_2$  in Ar. GHSV: 33 400  $\text{h}^{-1}$ . Ramp rate: 10 °C/min.

(increased outlet  $\text{SO}_x$  concentration) can be observed between 550 and 700 °C with increasing Pt load of the sample. The same trend is observed for the  $\text{SO}_2$  pre-exposed samples. However, comparing  $\text{SO}_x$  desorption from fresh and  $\text{SO}_2$  pre-exposed samples with the same Pt loading generally shows that more  $\text{SO}_x$  is released from the  $\text{SO}_2$  pre-exposed samples.

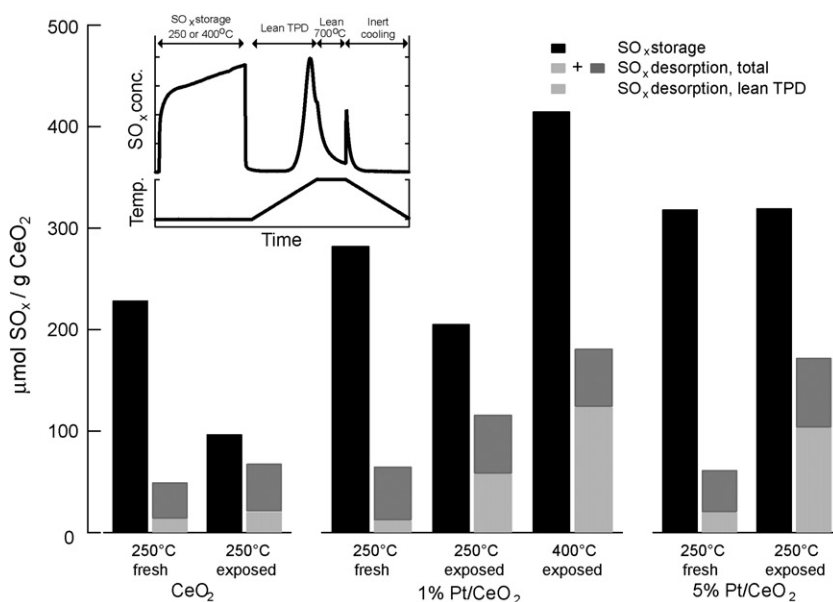
To investigate the influence of adsorption temperature on the  $\text{SO}_x$  storage and release capacity as well as the stability of the  $\text{SO}_x$  trap, repeated lean  $\text{SO}_x$  adsorption and TPD experiments were performed. The results from these experiments for the 1 wt.% Pt/ $\text{CeO}_2$  sample are shown in Figs. 5 and 6. The experiments were performed with the same 1 wt.% Pt/ $\text{CeO}_2$  sample used for the experiments shown in Figs. 3 and 4 as this sample already was exposed to large amounts of  $\text{SO}_2$  at both 250 and 400 °C. The  $\text{SO}_2$  adsorption was performed at two different temperatures following the sequence; 400, 250, 400 and 250 °C (with intermediate lean

$\text{SO}_x$ -TPD). The  $\text{SO}_x$  signals for the first and second  $\text{SO}_x$  adsorption and  $\text{SO}_x$  desorption coincide, revealing stable performance both at 250 and 400 °C. For lean  $\text{SO}_x$  adsorption, the outlet  $\text{SO}_x$  concentration is generally much lower when adsorption is performed at 400 °C as compared to at 250 °C. Considering the  $\text{SO}_x$ -TPD approximately twice as much  $\text{SO}_x$  are released after adsorption at 400 °C as compared to at 250 °C.

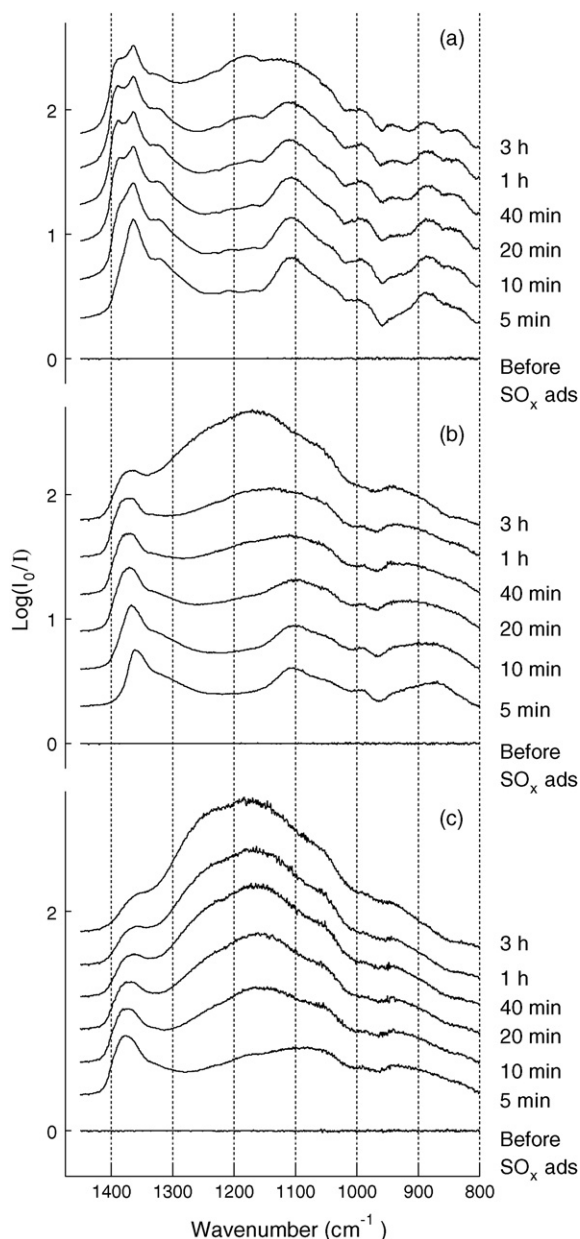
In Fig. 7, the amount of  $\text{SO}_x$  stored during the adsorption part of the experiments shown in Figs. 3 and 5 as well as the amount released during the regeneration part shown in Figs. 4 and 6 are summarised.

### 3.2. DRIFTS experiments

The results from the DRIFTS experiments where lean  $\text{SO}_x$  adsorption is performed at 250 °C for the  $\text{CeO}_2$  and 5 wt.% Pt/ $\text{CeO}_2$  samples and at 400 °C for the 5 wt.% Pt/ $\text{CeO}_2$  sample are displayed in Fig. 8 whereas results from the corresponding experiments for the  $\text{Al}_2\text{O}_3$  and 5 wt.% Pt/ $\text{Al}_2\text{O}_3$  samples are shown in Fig. 9. The spectra presented in Figs. 8 and 9 are subtractions of two spectra where the reference spectra are recorded after the pre-treatment at the temperature to be measured. The lean  $\text{SO}_x$  adsorption for the  $\text{CeO}_2$  sample at 250 °C results in several absorption bands between 800 and 1450  $\text{cm}^{-1}$  (cf. Fig. 8a). After 5 min of  $\text{SO}_2$  exposure, bands at 1365, 1325 (shoulder), 1215, 1175, 1100, 1000, 890 and 850 (shoulder) can be observed. Waqif et al. [15] have previously performed  $\text{SO}_2$  adsorption studies using FTIR for both high and low surface area  $\text{CeO}_2$  and assigned sharp bands between 1340 and 1400  $\text{cm}^{-1}$  to surface sulfates and broad bands near 1160  $\text{cm}^{-1}$  to bulk sulfates. The bands below 1050  $\text{cm}^{-1}$  in the present study are probably due to weakly bound surface sulfites or hydrogen sulfites [15]. After further  $\text{SO}_2$  exposure of the  $\text{CeO}_2$  sample and in agreement with the results from the study by Waqif et al. [15], a second shoulder evolve around 1390  $\text{cm}^{-1}$  in the surface sulfate region of the spectrum (cf. Fig. 8a). The broad band around 1175  $\text{cm}^{-1}$  with a shoulder at 1215  $\text{cm}^{-1}$  (attributed to bulk sulfates) is weak after 5 min of  $\text{SO}_2$  exposure, however the intensity of the band increases during the  $\text{SO}_2$  exposure. The positions of the bulk sulfate band and accompanying shoulder are



**Fig. 7.** Stored and released amount of  $\text{SO}_x$  for  $\text{CeO}_2$ -based  $\text{SO}_x$  traps calculated from the  $\text{SO}_x$  response during the  $\text{SO}_x$  adsorption and subsequent TPD experiments presented in Figs. 3–6. The total  $\text{SO}_x$  desorption is the sum of the release immediately after  $\text{SO}_2$  has been switched off before starting the TPD-ramp, the release during the lean-TPD, the release when keeping the temperature constant at 700 °C under lean conditions and the release during the inert cooling ramp.

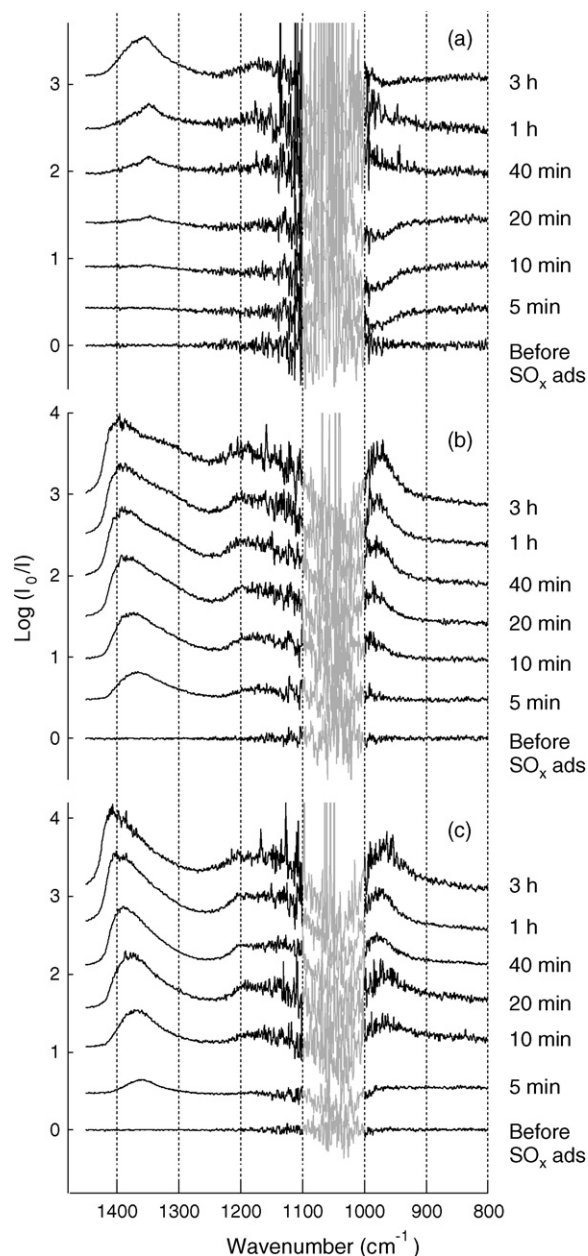


**Fig. 8.** DRIFTS results from lean  $\text{SO}_2$  exposure of (a)  $\text{CeO}_2$  at 250 °C, (b) 5 wt.% Pt/ $\text{CeO}_2$  at 250 °C and (c) 5 wt.% Pt/ $\text{CeO}_2$  at 400 °C. Feed composition during  $\text{SO}_2$  exposure: 300 ppm  $\text{SO}_2$  and 7%  $\text{O}_2$  in Ar. Feed composition during recording of spectra: 7%  $\text{O}_2$  in Ar. Total gas flow: 100 ml/min.

shifted during the  $\text{SO}_2$  exposure and are finally positioned at 1180 and 1235  $\text{cm}^{-1}$ , respectively, after 3 h.

The corresponding results for the Pt/ $\text{CeO}_2$  sample (cf. Fig. 8b) show absorption bands in the same regions as for the  $\text{CeO}_2$  sample, however, the bands are generally broader. In contrast to the surface sulfate band for the  $\text{CeO}_2$  sample, the band around 1370  $\text{cm}^{-1}$  for the Pt/ $\text{CeO}_2$  sample is not shifted towards higher wavenumbers during the  $\text{SO}_2$  exposure. Instead, this band becomes broader and the magnitude decreases slightly. The magnitude of the bulk sulfate bands (1180 and 1240  $\text{cm}^{-1}$ ) increases more rapidly for the Pt/ $\text{CeO}_2$  sample as compared to the  $\text{CeO}_2$  sample at 250 °C.

The increase of the adsorption temperature to 400 °C for the Pt/ $\text{CeO}_2$  sample (cf. Fig. 8c) results in an even faster increase in magnitude of the bulk sulfate bands whereas the magnitude of the



**Fig. 9.** DRIFTS results from lean  $\text{SO}_2$  exposure of (a)  $\text{Al}_2\text{O}_3$  at 250 °C, (b) 5 wt.% Pt/ $\text{Al}_2\text{O}_3$  at 250 °C and (c) 5 wt.% Pt/ $\text{Al}_2\text{O}_3$  at 400 °C. Feed composition during  $\text{SO}_2$  exposure: 300 ppm  $\text{SO}_2$  and 7%  $\text{O}_2$  in Ar. Feed composition during recording of spectra: 7%  $\text{O}_2$  in Ar. Total gas flow: 100 ml/min.

surface sulfate band formed after 5 min of  $\text{SO}_2$  exposure decreases more rapidly than at 250 °C.

Lean  $\text{SO}_2$  adsorption at 250 °C on the bare  $\text{Al}_2\text{O}_3$  sample (cf. Fig. 9a) results in fewer adsorption bands between 800 and 1450  $\text{cm}^{-1}$  as compared to the  $\text{CeO}_2$  sample. Due to non-diluted samples, the infrared radiation is completely absorbed by  $\text{Al}_2\text{O}_3$  between 1000 and 1100  $\text{cm}^{-1}$  with the present experimental setup. After 20 min of  $\text{SO}_2$  exposure, a weak band around 1350  $\text{cm}^{-1}$  evolves which increases during the exposure and shifts slightly to higher wavenumbers around 1360  $\text{cm}^{-1}$ . Saur et al. [20] have previously prepared surface sulfur species on  $\text{Al}_2\text{O}_3$  and  $\text{TiO}_2$  by various preparation routes. With FTIR spectroscopy, two accompanying bands at 1380 and 1045  $\text{cm}^{-1}$  were assigned to surface sulfates on  $\text{Al}_2\text{O}_3$ . The band between 1350 and 1360  $\text{cm}^{-1}$  in Fig. 9a originates most likely from surface sulfates on the  $\text{Al}_2\text{O}_3$

sample. In addition to the band around  $1360\text{ cm}^{-1}$ , a weak band at  $1160\text{ cm}^{-1}$  evolves for the  $\text{Al}_2\text{O}_3$  sample after approximately 1 h of  $\text{SO}_2$  exposure. This band was not observed by Saur et al. [20]. However, Mitchell et al. [21] have reported formation of an absorption band at  $1190\text{ cm}^{-1}$  after oxidising adsorbed  $\text{SO}_2$  species on  $\text{Al}_2\text{O}_3$ . The different results obtained in these two studies may originate from different sample preparation procedures and experimental setups. The IR spectrum by Mitchell et al. is very similar to the spectrum of bulk aluminium sulfate. The weak band around  $1160\text{ cm}^{-1}$  in Fig. 9a could therefore be due to bulk sulfates in the  $\text{Al}_2\text{O}_3$  sample, analogous to the bulk sulfate band around  $1180\text{ cm}^{-1}$  for  $\text{CeO}_2$ . However, in this study, the DRIFTS experiments with the  $\text{Al}_2\text{O}_3$  samples are performed to verify that the results obtained from the flow-reactor experiments are not effects of the binder, Boehmite. Hence, the assignment of the controversial  $1160\text{ cm}^{-1}$  band for the  $\text{Al}_2\text{O}_3$  samples is beyond the scope of this study. When  $\text{SO}_x$  adsorption is performed at  $250^\circ\text{C}$  for the Pt/ $\text{Al}_2\text{O}_3$  sample (cf. Fig. 9b), absorption bands can be observed in the same regions as for the  $\text{Al}_2\text{O}_3$  sample. However, the surface sulfate band is detected at slightly higher wavenumber,  $1370\text{ cm}^{-1}$ , already after 5 min of  $\text{SO}_2$  exposure and shifts to around  $1400\text{ cm}^{-1}$  during the experiment. The broad band around  $1160\text{ cm}^{-1}$  is also formed already after 5 min of  $\text{SO}_2$  exposure and the magnitude of both this band and the surface sulfate band increases during the experiment. When  $\text{SO}_x$  adsorption is performed at  $400^\circ\text{C}$  on the Pt/ $\text{Al}_2\text{O}_3$  sample (cf. Fig. 9c) no significant difference can be seen as compared to adsorption at  $250^\circ\text{C}$  on the same type of sample.

#### 4. Discussion

Ceria is an interesting material for regenerable  $\text{SO}_x$  traps owing to its basic properties and mobile oxygen ions. The results from flow-reactor experiments with synthetic gas compositions in this study indicate that  $\text{CeO}_2$  indeed is a suitable material for regenerable  $\text{SO}_x$  traps under lean conditions. Sulfur oxides are stored at temperatures between 200 and  $500^\circ\text{C}$  and released slightly above  $500^\circ\text{C}$  under lean conditions. In Fig. 1, lean  $\text{SO}_x$  adsorption for three different  $\text{SO}_x$  adsorbents is compared. Under these conditions, the Pt/ $\text{CeO}_2$  and Pt/ $\text{Al}_2\text{O}_3$  samples clearly show highest  $\text{SO}_x$  storage ability, i.e., slow increase in outlet  $\text{SO}_x$  concentration, as compared to the Pt/ $\text{Al}_2\text{O}_3$ :MgO and  $\text{Al}_2\text{O}_3$ :MgO samples. Note that the used inlet  $\text{SO}_2$  concentration, 100 ppm, is considerably higher than expected for real lean exhausts. During the subsequent  $\text{SO}_x$  desorption (cf. Fig. 2), the  $\text{Al}_2\text{O}_3$ :MgO-based samples release  $\text{SO}_x$  already below  $500^\circ\text{C}$ . Thus, these materials do not form sufficiently stable sulfur species to meet the specified requirements. The  $\text{Al}_2\text{O}_3$  and  $\text{CeO}_2$ -based samples do not release any significant amounts of  $\text{SO}_x$  below  $500^\circ\text{C}$ . At temperatures slightly above  $500^\circ\text{C}$  the  $\text{SO}_x$  desorption rate is highest for the Pt/ $\text{CeO}_2$  sample. It is also clear that addition of Pt to the  $\text{CeO}_2$  sample enhances the rate of both  $\text{SO}_x$  storage and release. On the basis of these results, we focus the remaining discussion on ceria and the influence of Pt on the  $\text{SO}_x$  storage and release kinetics under lean conditions emphasising the analogies with  $\text{NO}_x$  storage and release in  $\text{NO}_x$  storage catalysts.

Bazin et al. [22] have previously reported similar  $\text{SO}_x$  adsorption capacity under lean conditions at  $400^\circ\text{C}$  for  $\text{CeO}_2$  samples with and without Pt as presented in this study. In contrast to the results reported by Bazin et al., our results show that at  $250^\circ\text{C}$  the  $\text{SO}_x$  storage capacity of ceria samples under lean conditions is increased by including Pt on the samples, cf. Fig. 1. This is further emphasised when comparing the results for  $\text{SO}_x$  storage (cf. Figs. 3 and 7) for the different ceria samples, i.e.,  $\text{CeO}_2$ , 1 wt.% Pt/ $\text{CeO}_2$  and 5 wt.% Pt/ $\text{CeO}_2$ , clearly showing an increase in  $\text{SO}_x$  storage capacity with increased Pt content. The reason for this trend is most likely

connected to the importance of the  $\text{SO}_2$  oxidation kinetics over Pt and the subsequent adsorption on ceria as sulfates. This is analogous to  $\text{NO}$  oxidation which has shown to be crucial for efficient  $\text{NO}_x$  storage on BaO for  $\text{NO}_x$  storage catalysts [23,24]. Even though  $\text{SO}_3$  is the thermodynamically stable compound under lean conditions in the temperature interval of interest, i.e.,  $200\text{--}500^\circ\text{C}$ , the formation of  $\text{SO}_3$  is most likely kinetically limited in the lower temperature range. This is reflected by the low  $\text{SO}_x$  storage capacity for the pure ceria sample at  $250^\circ\text{C}$ . However, when Pt is added to the sample, the  $\text{SO}_3$  formation significantly increases and thus also the  $\text{SO}_x$  storage capacity. As ceria exhibits recognised dynamic redox behaviour [14] sulfates may form directly on ceria provided that the temperature is sufficiently high to overcome the activation barrier for this process. Thus, at elevated temperatures, sulfate formation on pure ceria may be sufficiently high to conceal additional effects of Pt on the  $\text{SO}_x$  storage kinetics. This most likely explains the difference between our measurements and the results reported by Bazin et al. where  $\text{SO}_x$  adsorption was performed at  $400^\circ\text{C}$ .

The DRIFTS results from  $\text{SO}_x$  adsorption on  $\text{CeO}_2$ -based samples show several absorption bands between  $500$  and  $1700\text{ cm}^{-1}$ . However, as the complete description of the origin of these bands is beyond the scope of the present study, we limit the discussion to the separation of surface and bulk sulfates. As the magnitude of the broad band around  $1180\text{ cm}^{-1}$  with a shoulder at  $1240\text{ cm}^{-1}$  increases more rapidly for the Pt/ $\text{CeO}_2$  sample as compared to the  $\text{CeO}_2$  sample at  $250^\circ\text{C}$ , we may conclude that Pt increases the rate of bulk sulfate formation. The increased rate of bulk sulfate formation is most likely due to increased rate of surface sulfate formation. Besides the kinetic effects of  $\text{SO}_3$  formation (i.e., higher  $\text{SO}_2$  oxidation rate over Pt), the increased rate of sulfate formation could also be connected to Pt-assisted oxygen transfer, i.e., spill-over of oxygen, from platinum to ceria sites with adsorbed  $\text{SO}_2$  in the close vicinity of the Pt crystallites. Independently of which route the surface sulfates are formed by, the formation will result in a considerable difference in sulfate concentration between the surface and bulk of ceria and thus a driving force for diffusion of sulfates into the bulk. The structure of ceria facilitates ion diffusion [14] and the exchange rate of ions between bulk and surface should be rather high. In this context it should be noted that the available surface area for  $\text{SO}_2$  adsorption is similar for the  $\text{CeO}_2$  and Pt/ $\text{CeO}_2$  samples as confirmed by the  $\text{N}_2$ -physisorption measurements (cf. Table 1).

When considering regeneration under lean conditions of the ceria-based samples, the amount of  $\text{SO}_x$  released during the temperature programmed desorption increases with increased Pt loading (0–5 wt.% Pt) of the samples (cf. Figs. 4 and 7). Because more  $\text{SO}_x$  is stored during the adsorption part of the experiment on  $\text{CeO}_2$  samples with higher Pt loading, it is not surprising that more  $\text{SO}_x$  also is released during the regeneration. The same trend is observed during the lean  $\text{SO}_x$ -TPD subsequent of adsorption at  $250$  and  $400^\circ\text{C}$  for the 1 wt.% Pt/ $\text{CeO}_2$  sample. A higher amount of  $\text{SO}_x$  is released after  $\text{SO}_x$  adsorption at  $400^\circ\text{C}$  as compared to at  $250^\circ\text{C}$ , as more  $\text{SO}_x$  is stored at  $400^\circ\text{C}$ . However, it is also possible to see a shift in the temperature where the desorption starts related to the Pt content of the  $\text{CeO}_2$  samples, especially for the fresh samples in Fig. 4, where the desorption of  $\text{SO}_x$  starts at  $550^\circ\text{C}$  for the 5 wt.% Pt/ $\text{CeO}_2$  sample and slightly above  $600^\circ\text{C}$  for the  $\text{CeO}_2$  sample. For the exposed samples, a shoulder on the desorption curve or even a desorption maximum below  $700^\circ\text{C}$  can be observed for the Pt-containing samples (cf. Figs. 4 and 6) whereas such shoulder is absent for the  $\text{CeO}_2$  samples below  $700^\circ\text{C}$ . These observations indicate that the increased  $\text{SO}_x$  desorption from  $\text{CeO}_2$  samples with higher Pt loading is not only due to the higher  $\text{SO}_x$  storage capacity of these samples. In analogy with  $\text{NO}_x$  storage catalysts [25], the

presence of Pt likely influences the release process of  $\text{SO}_x$ . As the sulfates appear to be fairly mobile in the sample, it is possible that reversed spill-over of sulfates from ceria sites close to Pt onto Pt sites can decrease the desorption temperature of these sulfur oxide species. The different  $\text{SO}_x$  release behaviour could also be owing to different adsorption sites available on the Pt-containing samples.

Comparison between the results for fresh and  $\text{SO}_2$  pre-exposed  $\text{CeO}_2$ -based samples indicates that there are different  $\text{SO}_x$  adsorption sites available on the samples. During the adsorption part of the experiment (cf. Figs. 3, 5 and 7) the  $\text{SO}_x$  adsorption capacity is higher for the fresh  $\text{CeO}_2$  and 1 wt.% Pt/ $\text{CeO}_2$  samples as compared to the exposed samples whereas no difference between fresh and exposed sample can be seen for the 5 wt.% Pt/ $\text{CeO}_2$  sample. During the regeneration, a higher amount  $\text{SO}_x$  is released from the exposed samples in all cases. The part of the total  $\text{SO}_x$  release which desorbs during the lean-TPD is also higher for the exposed samples in all cases and especially for the Pt-containing samples (cf. Fig. 7). From these results we conclude that not all storage sites on the  $\text{CeO}_2$ -based  $\text{SO}_x$  traps are possible to regenerate under lean conditions at below 700 °C. For the fresh sample, storage takes place on both regenerable and non-regenerable sites whereas for the  $\text{SO}_2$  pre-exposed sample, the storage almost exclusively takes place on regenerable sites. Because bulk sulfate formation is more rapid at 400 °C as compared to at 250 °C, it could be assumed that during the first temperature increase the formed surface sulfates migrate into the ceria bulk instead of being released from the sample. Therefore, the release of  $\text{SO}_x$  is low during the first regeneration. During the saturation step where the samples are exposed to high amounts of  $\text{SO}_2$  at 250 and 400 °C these bulk sites will probably be saturated or almost saturated. During the second regeneration, more  $\text{SO}_x$  is released as it is no longer possible for the sulfates to diffuse into the bulk during the temperature increase. Furthermore, the difference between  $\text{SO}_x$  storage capacity for fresh and pre-exposed sample is low or negligible when the Pt content of the sample is increased. The release around 600 °C, on the other hand, changes most for the samples with high Pt content. When increasing the Pt loading of the sample, the Pt/ $\text{CeO}_2$  contact area will most probably also increase. From these results it can be assumed that  $\text{SO}_x$  storage takes place more rapidly on storage sites close to Pt and that these storage sites are more easily regenerated than the corresponding sites located far away from Pt. Therefore, when increasing the Pt loading of the  $\text{CeO}_2$  samples, the number of regenerable  $\text{SO}_x$  storage sites will also increase.

## 5. Concluding remarks

Materials for regenerable  $\text{SO}_x$  traps with the ability to store and release  $\text{SO}_x$  under lean conditions but at different temperature intervals were investigated. Among the studied materials, Pt/ $\text{CeO}_2$  was recognised to be most promising. Under lean conditions, Pt/ $\text{CeO}_2$  shows the highest  $\text{SO}_x$  storage ability at 250 °C and most efficient release around 600 °C. It is found that the lean  $\text{SO}_x$  adsorption capacity at 250 °C and subsequent release in the temperature interval 500–700 °C increases with increased Pt loading (0, 1 and 5 wt.% Pt). Results from DRIFTS experiments reveal that  $\text{SO}_2$  adsorption on  $\text{CeO}_2$  samples under lean conditions proceeds via the formation of surface and bulk sulfates. The rate of bulk sulfate formation is higher for the Pt-impregnated  $\text{CeO}_2$  sample. Increasing the adsorption temperature, from 250 to 400 °C resulted in an increased amount of adsorbed  $\text{SO}_x$  for the 1 wt.% Pt/ $\text{CeO}_2$  sample. This is probably owing to faster  $\text{SO}_2$  oxidation kinetics at 400 °C and that the  $\text{SO}_3$  formation facilitates storage on  $\text{CeO}_2$ . An increased adsorption temperature from 250 to 400 °C is

also found to yield more rapid bulk sulfate formation for the Pt/ $\text{CeO}_2$  sample.

Moreover,  $\text{SO}_x$  adsorption and regeneration of fresh and  $\text{SO}_2$  pre-exposed samples were compared. Generally, a lower amount of  $\text{SO}_x$  can be stored on the pre-exposed samples but for the 5 wt.% Pt/ $\text{CeO}_2$  sample, no significant difference between fresh and pre-exposed samples can be observed. During the subsequent regeneration, more  $\text{SO}_x$  are released from the exposed samples in all cases. These results indicate that some of the storage sites on the  $\text{CeO}_2$ -based samples are not possible to regenerate at 700 °C or below under lean conditions. During the pre-exposure, the  $\text{SO}_x$  storage capacity decreases less and the  $\text{SO}_x$  release increases most for the samples with higher Pt loading. This indicates that Pt increases the number of regenerable sites on the  $\text{SO}_x$  trap or that Pt increases the formation of a certain sulfur species that both forms faster during adsorption conditions and releases faster during desorption conditions.

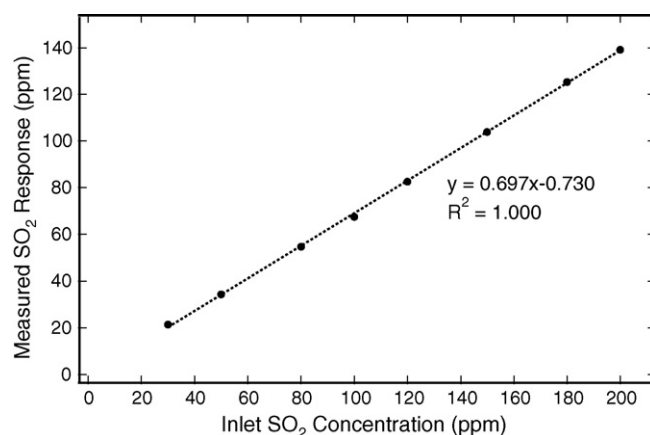
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## Appendix A

### A.1. Continuous monitoring of total $\text{SO}_x$ concentration in a lean gas flow

To evaluate the performance of model  $\text{SO}_x$  traps in a flow-reactor setup, continuous monitoring of total  $\text{SO}_x$  concentration in the gas flow is necessary. A method facilitating analysis of the total  $\text{SO}_x$  concentration in a lean gas flow using a  $\text{SO}_2$  analyser has previously been reported by D. McLaughlin et al. at the Taylor conference in Belfast 2004. Following this method with only minor modifications, the gas flow was passed over an oxidation catalyst before introduced to the  $\text{SO}_2$  analyser (non-dispersive IR, Mairhak



**Fig. A.1.** Measured  $\text{SO}_2$  response during calibration with various inlet  $\text{SO}_2$  concentrations. The gas flow is passed over an oxidation catalyst heated to 675 °C before introduced to the  $\text{SO}_2$  analyser. Feed composition: 30, 50, 80, 100, 120, 150, 180 or 200 ppm  $\text{SO}_2$  and 7%  $\text{O}_2$  in Ar.



UNOR 610). The oxidation catalyst (Pt/SiO<sub>2</sub>) was heated to 675 °C which is the equilibrium temperature for the composition 50% SO<sub>2</sub>/50% SO<sub>3</sub> in oxygen excess. Due to instrumental cross sensitivity for SO<sub>2</sub> and SO<sub>3</sub>, about 70% of the total amount of SO<sub>x</sub> was detected as SO<sub>2</sub> with the present experimental setup (cf. Fig. A.1). From the measured SO<sub>2</sub> response, the total SO<sub>x</sub> concentration was finally estimated. In order to ensure the performance of the oxidation catalyst and the IR instrument, calibration with 100 ppm SO<sub>2</sub> and 7% O<sub>2</sub> in Ar was performed before as well as after each experiment.

## References

- [1] S. Matsumoto, *Cattech* 4 (2001) 102–109.
- [2] N. Takahashi, H. Shinjoh, T. Iijima, T. Suzuki, K. Yamazaki, K. Yokota, H. Suzuki, N. Miyoshi, S. Matsumoto, T. Tanizawa, T. Tanaka, S.-s. Tateishi, K. Kasahara, *Catal. Today* 27 (1996) 63–69.
- [3] A. Amberntsson, B. Westerberg, P. Engström, E. Fridell, M. Skoglundh, *Studi. Surf. Sci. Catal.* 126 (1999) 317–324.
- [4] C. Sedlmair, K. Seshan, A. Jentys, J.A. Lercher, *Catal. Today* 75 (2002) 413–419.
- [5] J. Dawody, M. Skoglundh, L. Olsson, E. Fridell, *J. Catal.* 234 (2005) 206–218.
- [6] S. Matsumoto, Y. Ikeda, H. Suzuki, M. Ogai, N. Miyoshi, *Appl. Catal. B: Environ.* 25 (2000) 115–124.
- [7] G. Centi, G. Fornasari, C. Gobbi, M. Livi, F. Trifiro, A. Vaccari, *Catal. Today* 73 (2002) 287–296.
- [8] G. Fornasari, R. Glöckler, M. Livi, A. Vaccari, *Appl. Clay Sci.* 29 (2005) 258–266.
- [9] L. Limousy, H. Mahzoul, J.F. Brilhac, P. Pilot, F. Garin, G. Maire, *Appl. Catal., B: Environ.* 42 (2003) 237–249.
- [10] H. Dathe, A. Jentys, J.A. Lercher, *Phys. Chem. Chem. Phys.* 7 (2005) 1283–1292.
- [11] L. Li, D.L. King, *Ind. Eng. Chem. Res.* 44 (2005) 7388–7397.
- [12] K. Tikhomirov, O. Kröcher, M. Elsener, M. Widmer, A. Wokaun, *Appl. Catal., B: Environ.* 67 (2006) 160–167.
- [13] A. Amberntsson, M. Skoglundh, S. Ljungström, E. Fridell, *J. Catal.* 217 (2003) 253–263.
- [14] A. Trovarelli, *Catalysis by Ceria and Related Materials*, Catalytic Science Series, Imperial College Press, London, 2005.
- [15] M. Waqif, P. Bazin, O. Saur, J.C. Lavalley, G. Blanchard, O. Touret, *Appl. Catal., B: Environ.* 11 (1997) 193–205.
- [16] A.E. Palomares, J.M. López-Nieto, F.J. Lázaro, A. López, A. Corma, *Appl. Catal., B: Environ.* 20 (1999) 257–266.
- [17] S. Brunauer, P.H. Emmett, E. Teller, *J. Am. Chem. Soc.* 60 (1938) 309–319.
- [18] J. Dawody, M. Skoglundh, S. Wall, E. Fridell, *J. Mol. Catal. A: Chem.* 225 (2005) 259–269.
- [19] D. McLaughlin, F. Meunier, J.P. Breen, R. Burch (unpublished).
- [20] O. Saur, M. Bensitel, A.B.M. Saad, J.C. Lavalley, C.P. Tripp, B.A. Morrow, *J. Catal.* 99 (1986) 104–110.
- [21] M.B. Mitchell, V.N. Sheinker, M.G. White, *J. Phys. Chem.* 100 (1996) 7550–7557.
- [22] P. Bazin, O. Saur, J.C. Lavalley, G. Blanchard, V. Visciglio, O. Touret, *Appl. Catal., B: Environ.* 13 (1997) 265–274.
- [23] E. Fridell, M. Skoglundh, B. Westerberg, S. Johansson, G. Smedler, *J. Catal.* 183 (1999) 196–209.
- [24] L. Olsson, H. Persson, E. Fridell, M. Skoglundh, B. Andersson, *J. Phys. Chem. B* 105 (2001) 6895–6906.
- [25] I. Nova, L. Lietti, L. Castoldi, E. Tronconi, P. Forzatti, *J. Catal.* 239 (2006) 244–254.